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Comparison of Penetration Efficiency in Axial and Planer Symmetries

Y. Partom Institute for Advanced Technology The University of Texas at Austin

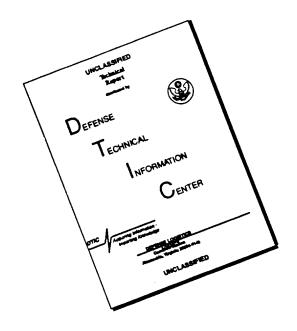
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November 1993

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Yehuda Partom

Stephan Bless

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Comparison of Penetration Efficiency in Axial and Planer Symmetries

by Yehuda Partom

It has been known for some time that, for a given target, a flat cross section projectile would penetrate deeper than a circular cross section projectile, other factors being equal. This invoked the idea that a cruciform cross section projectile would have an advantage over the circular cross section projectile.

To simulate the penetration process of a cruciform projectile, we need to employ a 3D wavecode. As such a code is not yet available to us, we conducted a preparatory investigation using the 2D wavecode AUTODYN2D. We ran identical penetration problems in axial and planar (2D strain) symmetries. The planar symmetry projectile can be regarded as an extreme case of a flat projectile. This means that if indeed a flat projectile is more efficient than a circular projectile, the flat projectile (being laterally finite) always penetrates less than the equivalent planar symmetry projectile. Therefore, the basic idea of the investigation is as follows. If the simulations show that a planar symmetry projectile has sufficient advantage over the equivalent axial symmetry projectile, then a cruciform projectile may be a promising design.

In all simulations we used a steel target and steel or tungsten alloy L/D = 10 projectiles. We used a Mie-Gruneisen EOS referenced to the shock adiabat with the parameters listed in Table 1 below:

Table 1 **EOS Parameters**

	Steel	Tungsten Alloy
ρο	7.85 g/cc	17.3 g/cc
C _o	3.57 mm/µs	4.03
S	1.92	1.24
Γ_{o}	1.7	1.7
P_{min}	-2 GPa	-2 GPa

where ρ = density, C_{\circ} , S are the shock velocity particle velocity relation parameters, Γ_{\circ} = Gruneisen parameter and P_{min} is the spall strength.

For the stress deviator we used a constant shear modulus G and a vo⁻⁻ vises yield surface with a constant flow stress Y as shown in Table 2:

Table 2
Shear Stress Parameters

	Steel	⊿ngsten Alloy
G	80 Gpa	140 GPa
Y	1 GPa	2GPa

Projectile dimensions were D/2 = 5 mm, L = 100 mm; the Euler cell dimensions were 1 x1 mm. Target dimensions varied according to symmetry, projectile material (steel or Tungsten alloy) and velocity. Specifically, in the planar symmetry case, we observed that very large target dimensions are needed to exert a reasonable amount of confinement. Target dimensions used in the various cases are listed in Table 3.

Table 3 **Target Dimensions**

No.	Projectile Material	Symmetry	Velocity (km/s)	D _t /2 (mm)	L _t (mm)
1	Steel	Circular	1.5	100	100
2	it	II	2.0	100	200
3	Ħ	11	2.5	100	200
4	II	planar	1.5	250	250
5	II	์ ม	2.0	280	280
6	11	II	2.5	280	280
7	tungsten alloy	circular	1.5	100	150
8	"	planar	1.5	280	280

In the axial symmetry runs, cell dimensions in the target were also 1 x 1 mm. In the planar symmetry runs, cell dimensions were 1 x 1 mm for x < 100 mm and y < 100 mm, where x = 0 is the impact surface and y = 0 is the (planar) symmetry axis. Beyond x = 100 mm and

y = 100 mm, cell dimensions grew progressively. There were 8 runs as shown in Table 3. The initial plan included 6 runs: 2 projectile materials (steel and tungsten alloy), 2 velocities (1.5 and 2.5 km/s (only for the steel projectile), and 2 symmetries (axial and planar); however, the higher velocity runs provided an unexpected result. To convince ourselves that there was no error, we did 2 additional runs with the steel projectile at an intermediate velocity (2 km/s). To document the runs we show plots of material status and velocity vectors (near the projectile target interface) in Appendix A (included only in 2 copies of this report). The plots are snapshots every 200 cycles. They are arranged according to the run numbers in Table 3. To analyze the results of these runs, we show interface velocity and projectile tail velocity history plots and penetrationerosion curves.

The velocity plots are shown in Figs. 1.1 to 1.4.

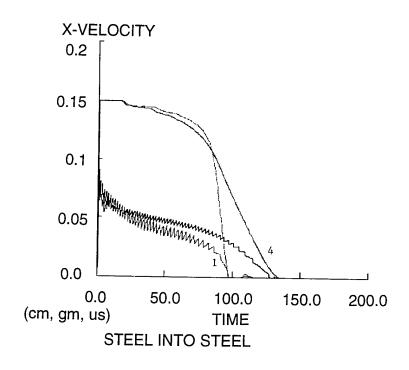


Fig. 1.1. Runs 1 and 4.

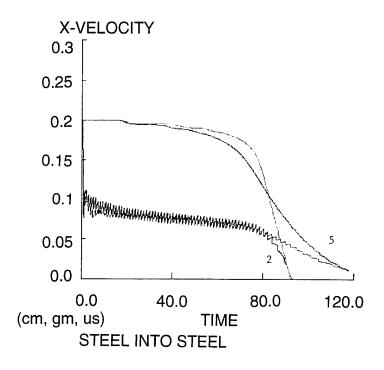


Fig. 1.2. Runs 2 and 5.

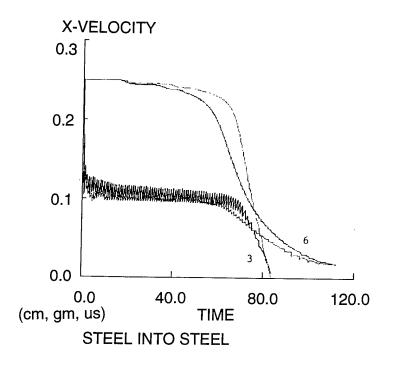


Fig. 1.3. Runs 3 and 6.

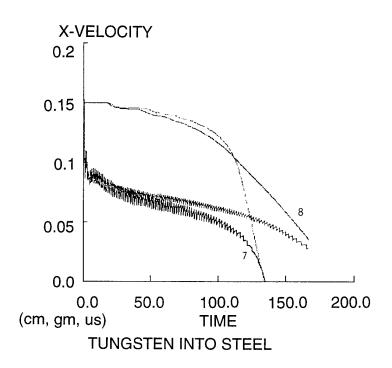


Fig. 1.4. Runs 7 and 8.

Figure 1.1 to 1.4 Interface velocity and projectile tail velocity histories (1.1 is for runs 1 and 1.2 is for runs 2 and 5, 1.3 is for runs 3 and 6, and 1.4 is for runs 7 and 8).

Figs. 1.1 and 1.4 are for V = 1.5 km/s for steel into steel and for tungsten alloy into steer respectively. In both figures, we see that the penetration velocity for planar symmetry is higher this is not the case for V = 2 km/s and V = 2.5 km/s. In Fig. 1.2 (V = 2 km/s, steel into steel), V = 2.5 km/s, steel into steel), we see that the penetration velocity for planar symmetry is high than that for axial symmetry. This shows that a planar symmetry projectile has an advantage low velocities but loses its advantage with increasing velocity. We see this behavior even mo clearly in the penetration-erosion curves shown in Figs. 2.1 to 2.4.

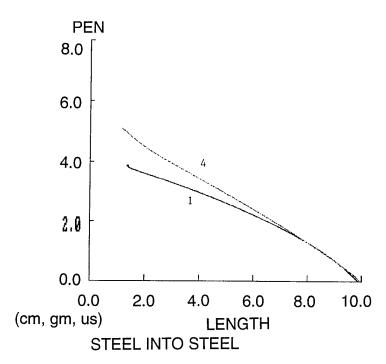


Fig. 2.1. Runs 1 and 4.

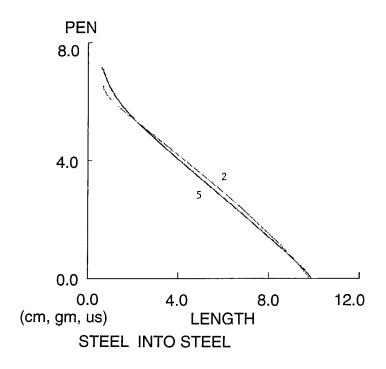


Fig. 2.2. Runs 2 and 5.

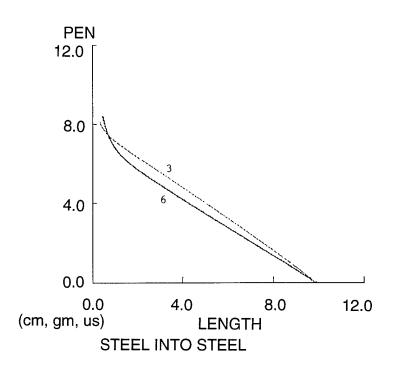


Fig. 2.3. Runs 3 and 6.

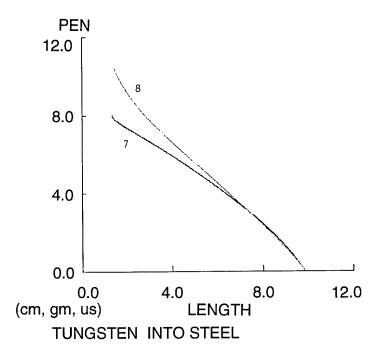


Fig. 2.4. Runs 7 and 8.

Figs. 2.1 to 2.4. Penetration-erosion curves (2.1 is for runs 1 and 4, 2.2 is for runs 2 and 5, 2.3 is for runs 3 and 6, and 2.4 is for runs 7 and 8).

Figs 2.1 and 2.4 are for V = 1.5 km/s, for steel into steel and tungsten alloy into steel, respectively. We see that in both cases, the planar symmetry projectile has out 30% advantage over the axial symmetry projectile. In Figs. 2.2 and 2.3 we see that for $V = \frac{1.5}{100}$ km/s the advantage decreases to about 10%, and for V = 2.5 km/s it decreases to about 5%. The penetration results (Pi) for all 8 runs are given in Table 4.

Table 4 **Penetration Results**

Run No.	V(km/s)	Pf/Lo	Proj. Mat.
1	1.5	0.38	steel
2	1.5	0.51	н
3	2.0	0.65	н
4	2.0	0.71	11
5	2.5	0.80	ii .
6	2.5	0.84	II .
7	1.5	0.80	Tungsten alloy
8	1.5	1.04	н

Observing the plots in Appendix A, we notice substantial differences in the penetration process characteristics between the two symmetries.

The first difference has to do with lateral confinement. In Fig. 3, we show plots of material status at 1000 cycles for runs 7 and 8 (tungsten alloy into steel at 1.5 km/s). We see that while for axial symmetry a target of Dt/2 = 100 mm, Lt = 150 mm provides practically full confinement, for planar symmetry, even a target as large as Dt/2 = 280 mm, Lt = 280 is not enough, as the upper and back boundaries have moved. We also see that the lip around the crater on the front boundary is much larger for planar symmetry. It's about 5 times larger (in linear dimensions).

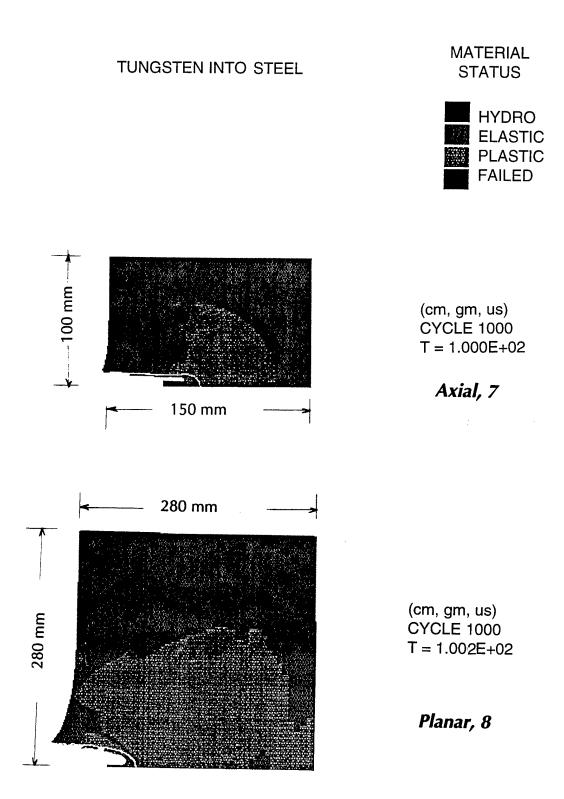


Fig. 3. Material status for runs 7 and 8 at 1000 cycles (\sim 100 μ s).

The second difference has to do with crater dimensions. Both size and shape are different. As an example, we show in Fig. 4 detailed plots of the inner part of the crater in runs 7 and 8 at 1000 cycles. We see that while for axial symmetry the crater diameter is approximately constant and is about 1.8 times the projectile diameter (at 1.5 km/s) for planar symmetry the crater width is not constant, and at the entrance boundary it is about five times the rojectile width. At this time, we don't have quantitative understanding or valid engineering odels to account for these differences.

IUNGILM IMINTO STEEL

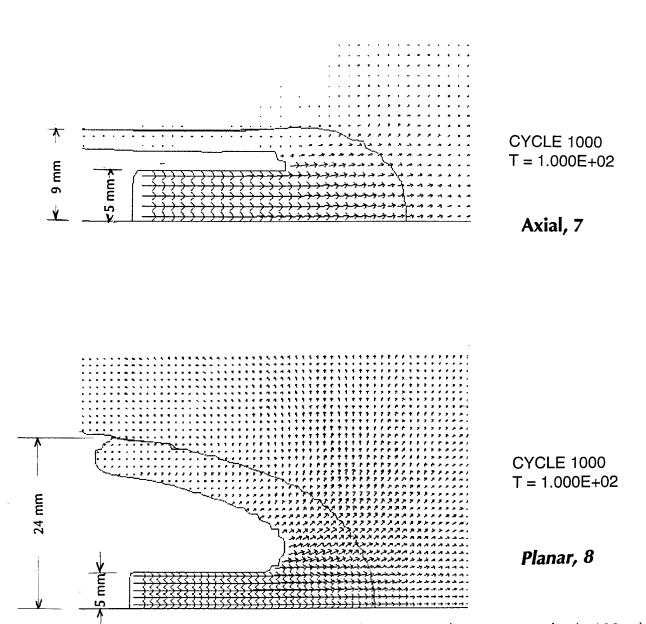


Fig. 4. Crater geometry and velocity vectors for runs 7 and 8 at 1000 cycles ($\sim 100~\mu s$).

Conclusions

We used AUTODYN2D to simulate penetration of steel and tungsten alloy projectiles into steel targets for axial and planar symmetries. The purpose was to see to what extent the planar projectiles have an advantage over circular projectiles.

We found that:

- Planar projectiles penetrate more than circular projectiles at low velocities (1.5 km/s).
- Planar projectiles lose their advantage with increasing velocity.

Velocity km/s	Advantage of Planar Projectiles
1.5	30%
2.0	10%
2.5	5%

- Much larger target dimensions are needed for full confinement of planar projectiles.
- Craters created by planar projectiles are much wider and their width is not constant.

Acknowledgments

This work was supported by the U.S. Army Armament Research, Development and Engineering Center (ARDEC) under contract DAAA21-90-D-0009.

Appendix A

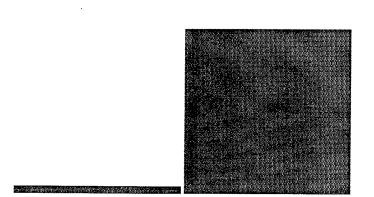
Material status and velocity vector plots for runs 1 to 8.

Appendix A is included in only 2 copies of this report.

Runs 1 to 8 are characterized in Table 3.

Appendix A1

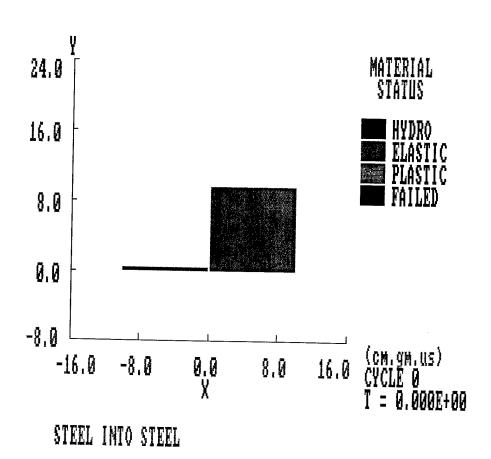
Plots for run No. 1 Steel projectile Axial symmetry 1.5 km/s

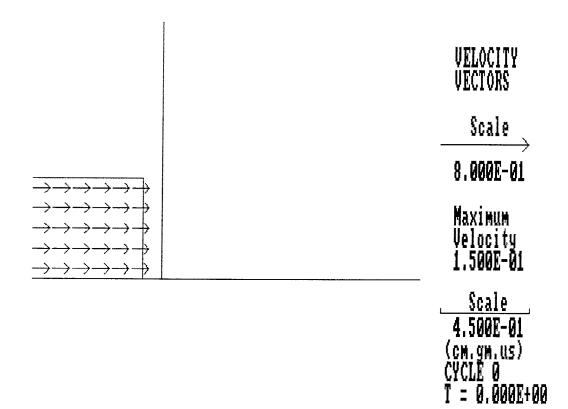


MATERIAL STATUS

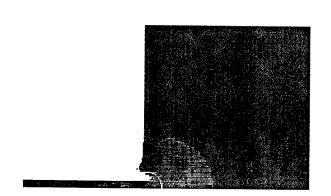


(cm.gm.us) CYCLE 0 T = 0.000E+00





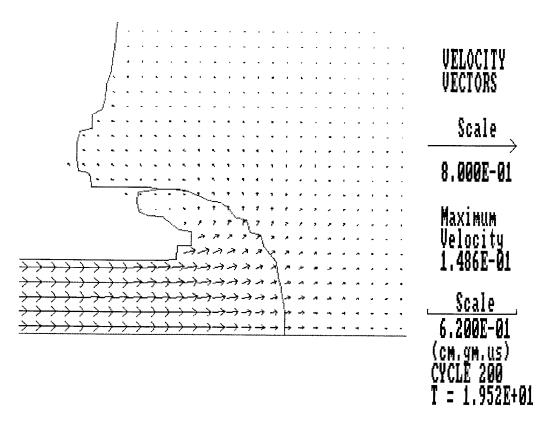
STEEL INTO STEEL



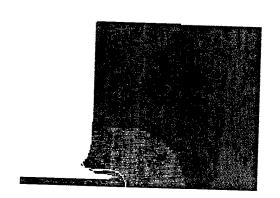


(cm.gm.us) CYCLE 200 T = 1.952E+01

STEEL INTO STEEL



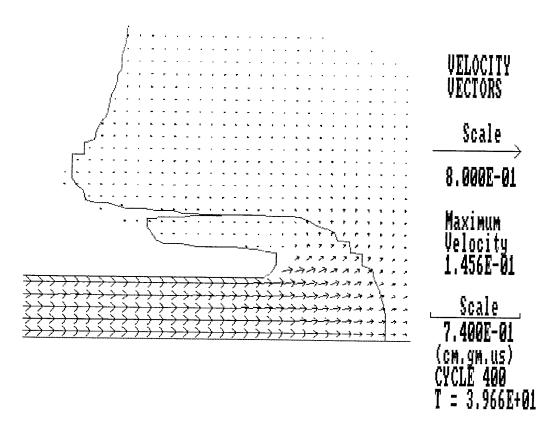
STEEL INTO STEEL



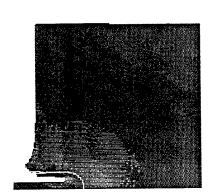


(cm.gm.us) CYCLE 400 T = 3.966E+01

STEEL INTO STEEL

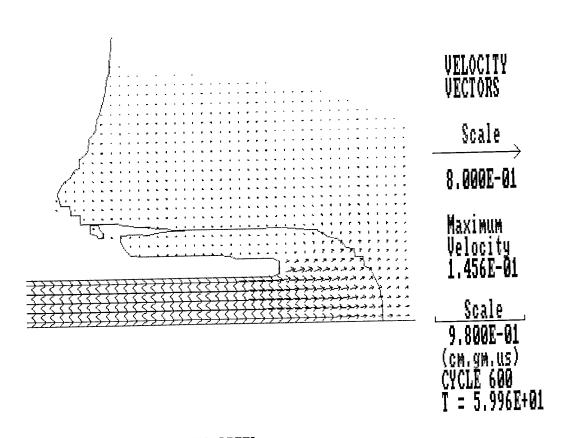


STEEL INTO STEEL

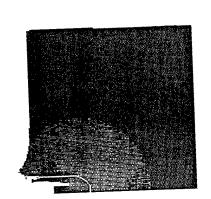




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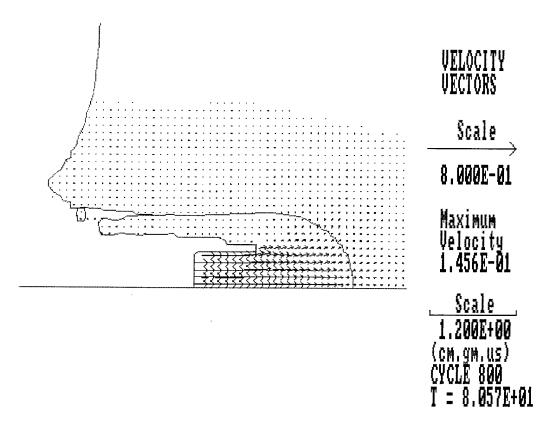
STEEL INTO STEEL



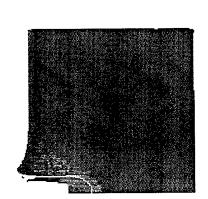


(cm.gm.us) CYCLE 800 T = 8.057E+01

STEEL INTO STEEL

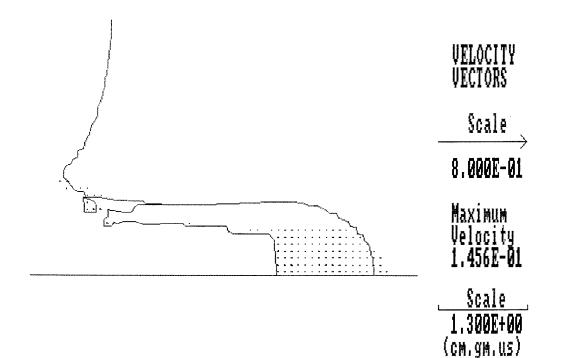


STEEL INTO STEEL

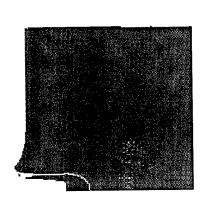


MATERIAL STATUS HYDRO ELASTI(

(cm.gm.us) CYCLE 1000 T = 1.032E+02

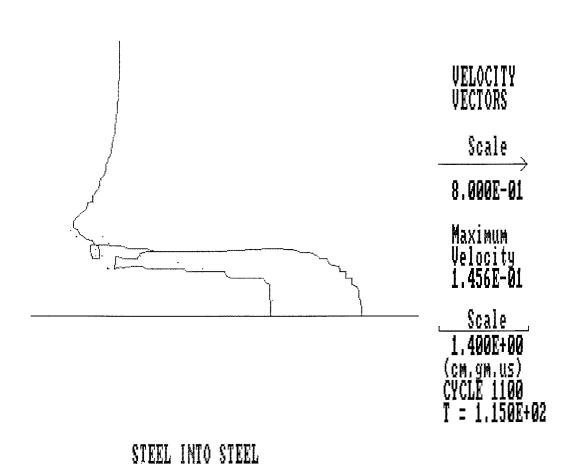


STEEL INTO STEEL





(cm.gm.us) CYCLE 1100 T = 1.150E+02

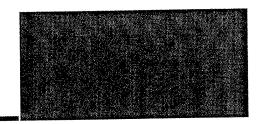


Appendix A2

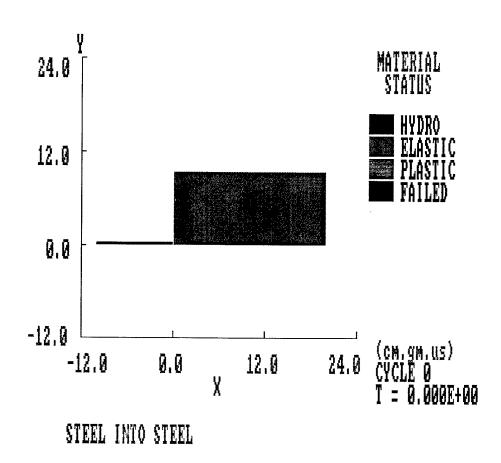
Plots for run No. 2 Steel projectile Axial symmetry 2.0 km/s

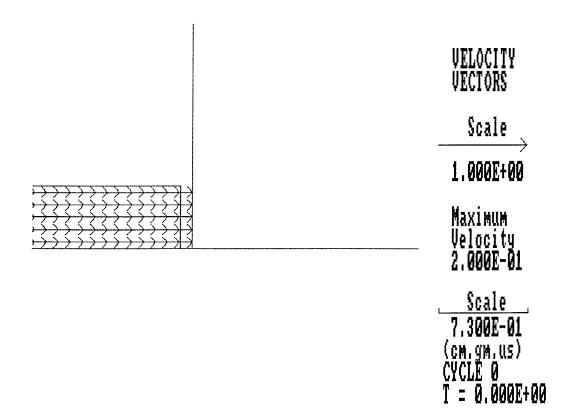




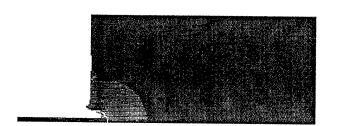


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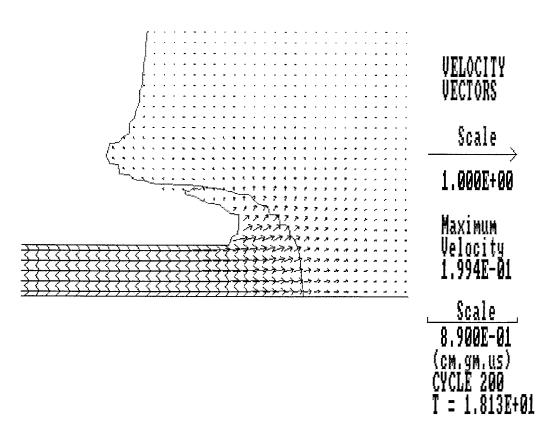


STEEL INTO STEEL





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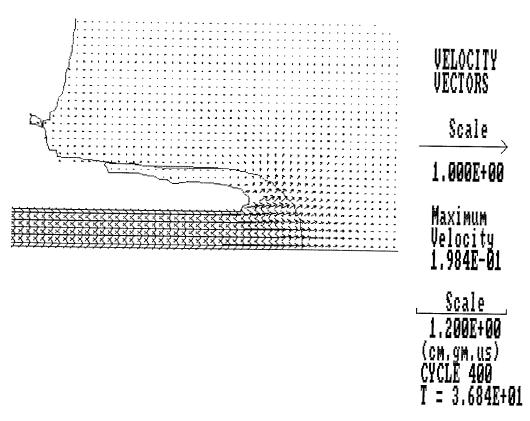


STEEL INTO STEEL





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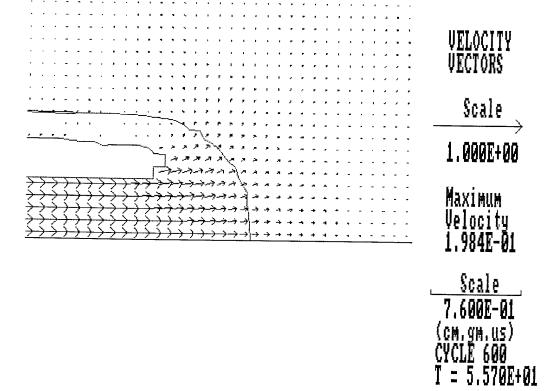


STEEL INTO STEEL

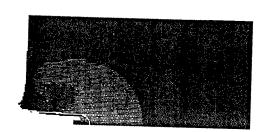




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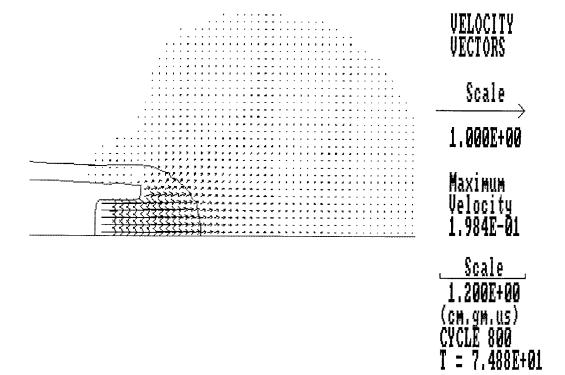


STEEL INTO STEEL





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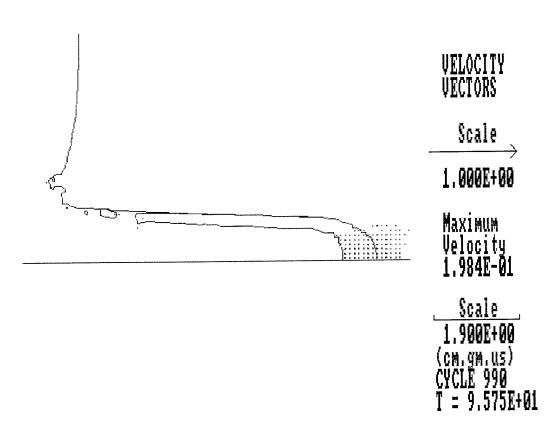


STEEL INTO STEEL





(cm.gm.us) CYCLE 990 T = 9.575E+01



STEEL INTO STEEL

Appendix A3

Plots for run No. 3 Steel projectile Axial symmetry 2.5 km/s



MATERIAL STATUS HYDRO ELASTIC PLASTIC

(cm.gm.us) CYCLE 0 T = 0.000E+00

VELOCITY VECTORS

Scale

2.000E+00

Maximum
Velocity
2.500E-01

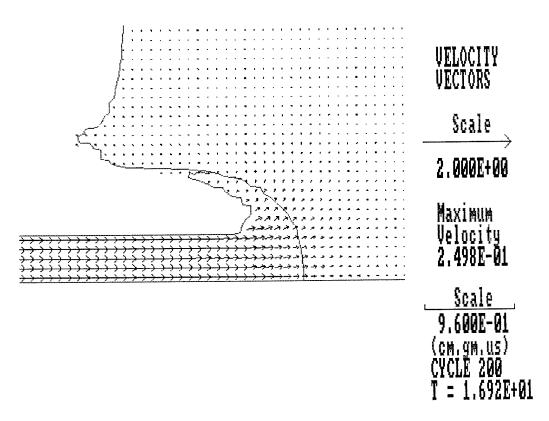
Scale
1.000E+00
(cm.gm.us)
CYCLE 0
T = 0.000E+00

STEEL INTO STEEL





(cm.gm.us) CYCLE 200 T = 1.692E+01



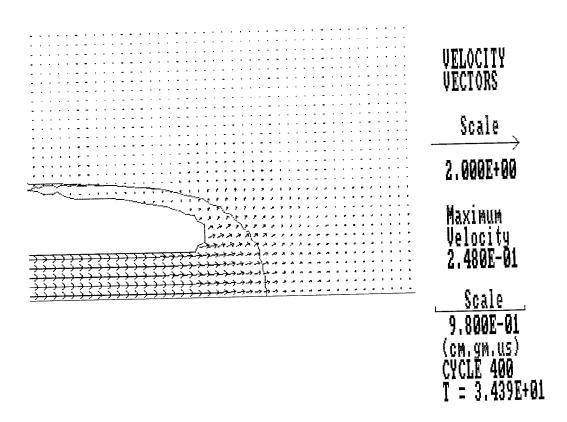
STEEL INTO STEEL







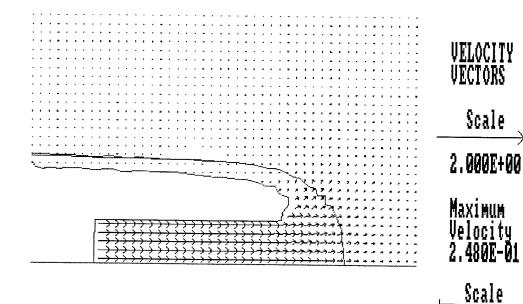
(cm.gm.us) CYCLE 400 T = 3.439E+01



STEEL INTO STEEL



(cm.gm.us) CYCLE 600 T = 5.201E+01



STEEL INTO STEEL

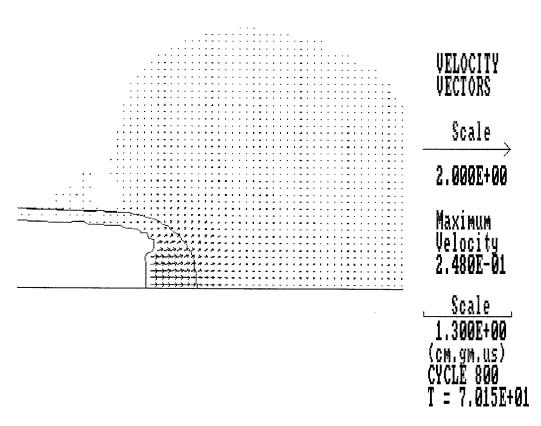
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MATERIAL STATUS



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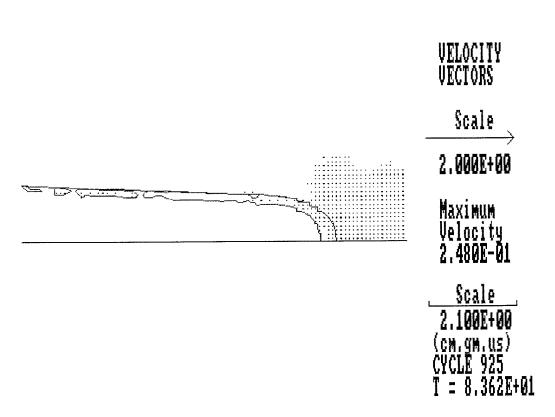
STEEL INTO STEEL



MATERIAL STATUS



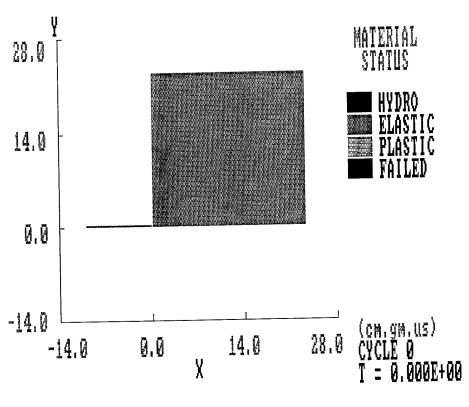
(cm.gm.us) CYCLE 925 T = 8.362E+01



STEEL INTO STEEL

Appendix A4

Plots for run No. 4 Steel projectile Planar symmetry 1.5 km/s



STEEL INTO STEEL PLANAR

VELOCITY
VECTORS

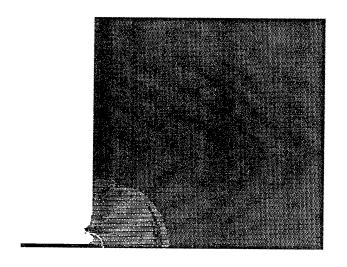
Scale

8.000E-01

Maximum
Velocity
1.500E-01

(cm, gm, us)
CYCLE 0
T = 0.000E+00

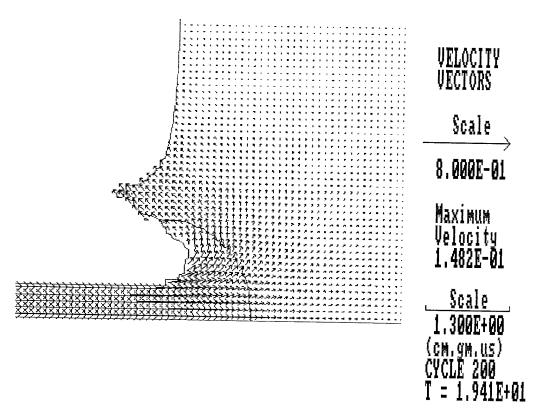
STEEL INTO STEEL PLANAR



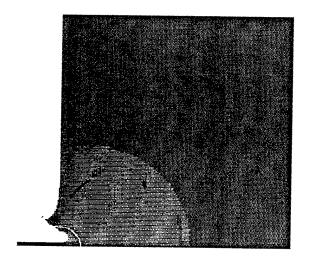


(cm.gm.us) CYCLE 200 T = 1.941E+01

STEEL INTO STEEL PLANAR



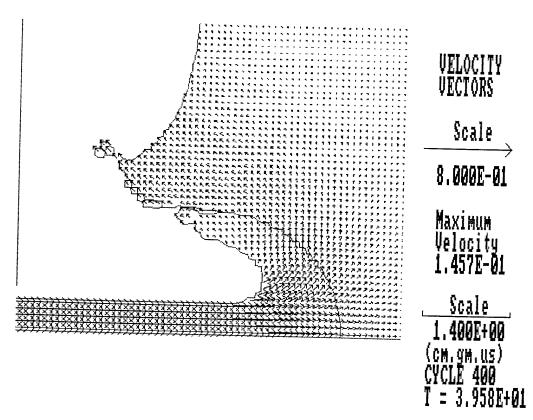
STEEL INTO STEEL PLANAR



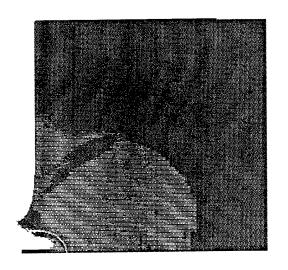
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 400 T = 3.958E+01

STEEL INTO STEEL PLANAR



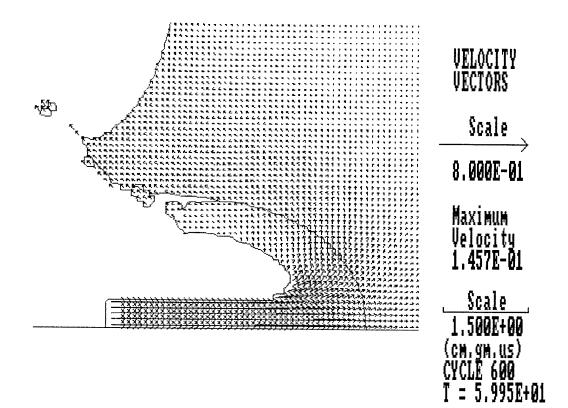
STEEL INTO STEEL PLANAR



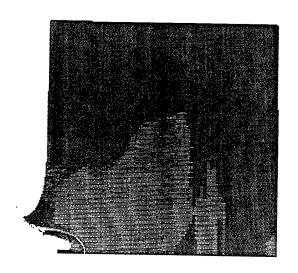
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 600 T = 5.995E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

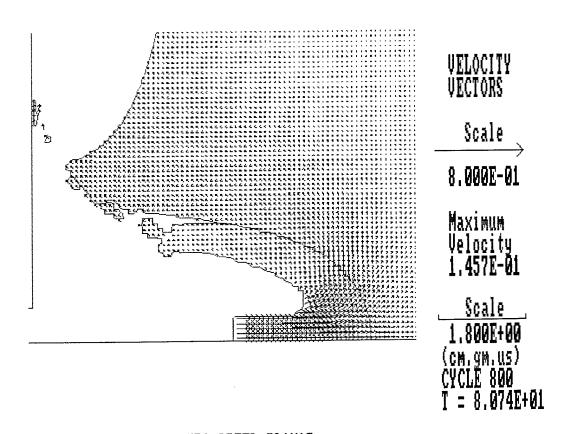


MATERIAL STATUS

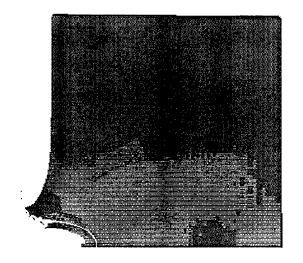


(cm.gm.us) CYCLE 800 T = 8.074E+01

STEEL INTO STEEL PLANAR



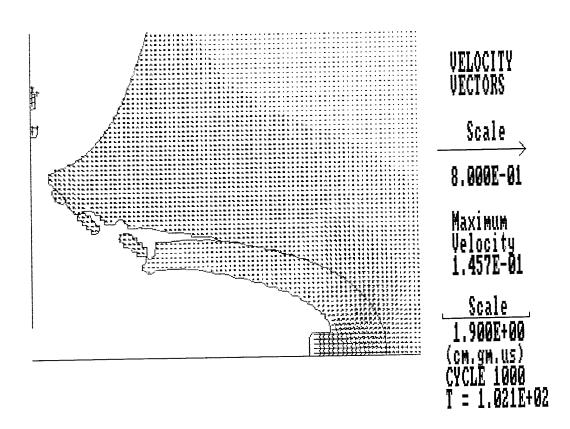
STEEL INTO STEEL PLANAR



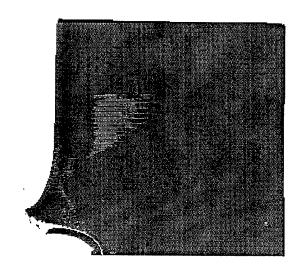


(cm.gm.us) CYCLE 1000 T = 1.021E+02

STEEL INTO STEEL PLANAR



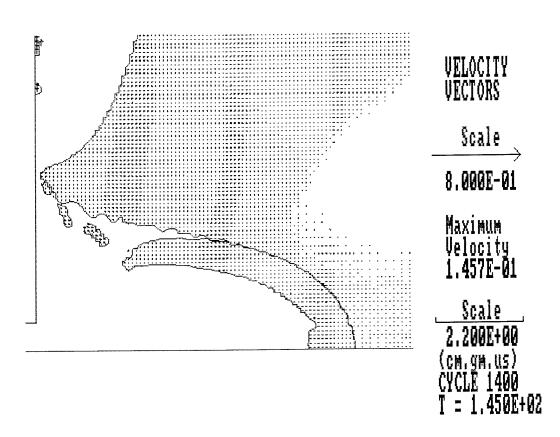
STEEL INTO STEEL PLANAR



HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 1400 T = 1.450E+02

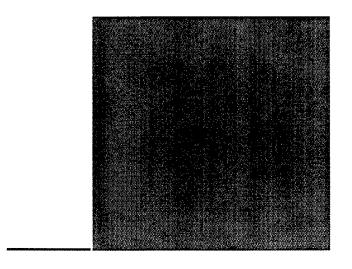
STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

Appendix A5

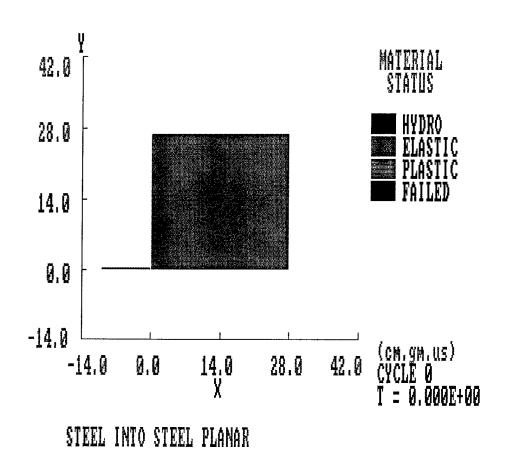
Plots for run No. 5 Steel projectile Planar symmetry 2.0 km/s





(cm.gm.us) CYCLE 0 T = 0.000E+00

STEEL INTO STEEL PLANAR



VELOCITY VECTORS

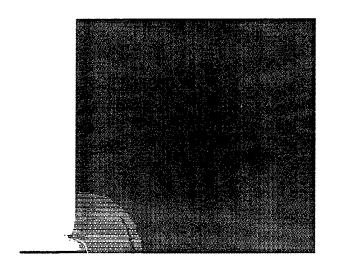
Scale

1.000E+00

Maximum Velocity 2.000E-01

Scale 6.800E-01 (cm.gm.us) CYCLE 0 T = 0.000E+00

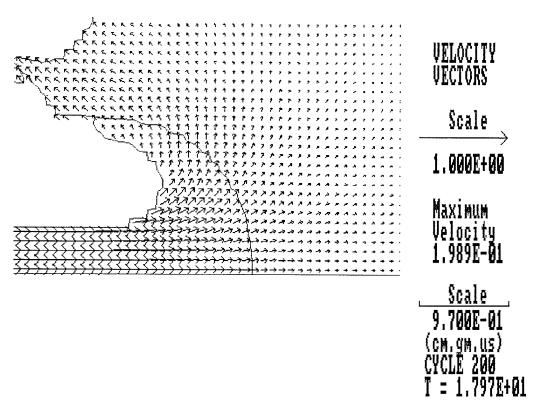
STEEL INTO STEEL PLANAR



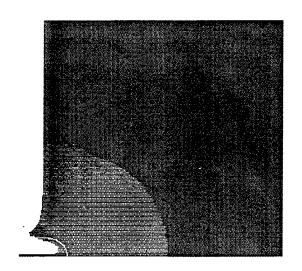


(cm.gm.us) CYCLE 200 T = 1.797E+01

STEEL INTO STEEL PLANAR



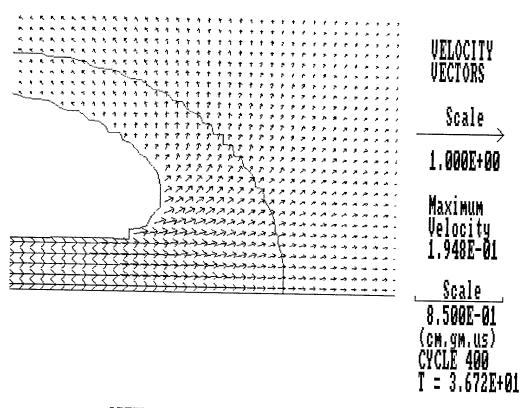
STEEL INTO STEEL PLANAR



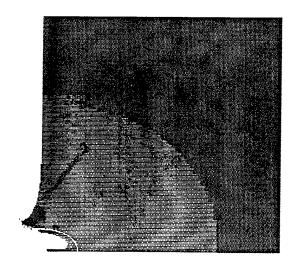
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 400 T = 3.672E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

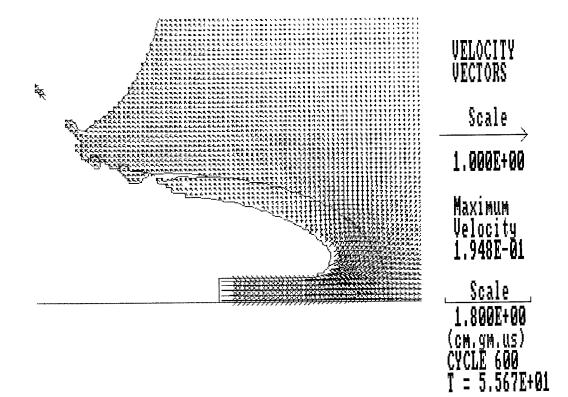


MATERIAL STATUS

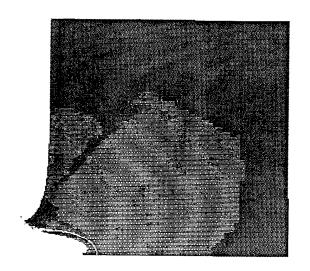


(cm.gm.us) CYCLE 600 T = 5.567E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

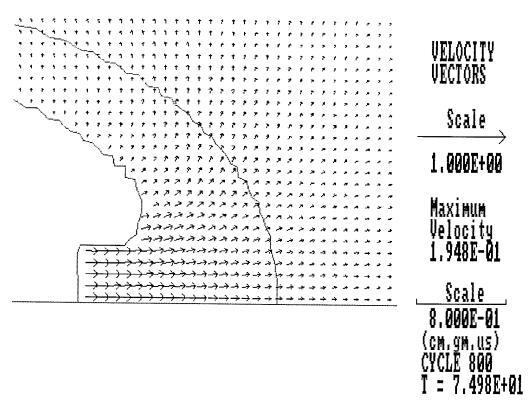


MATERIAL STATUS

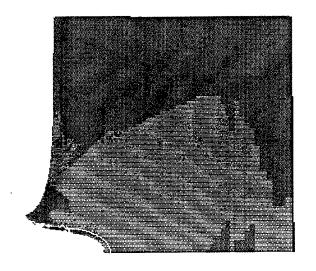
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 800 T = 7.498E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

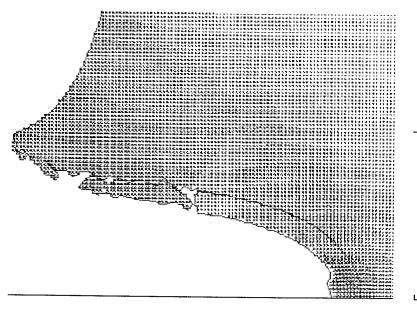


MATERIAL . STATUS

HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 1000 T = 9.608E+01

STEEL INTO STEEL PLANAR



VELOCITY VECTORS

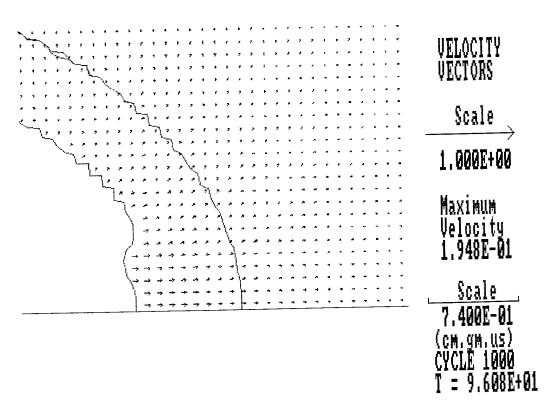
Scale

1.000E+00

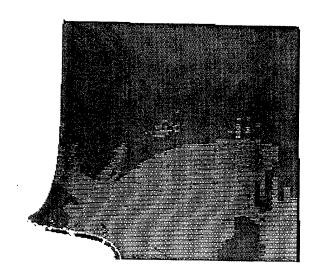
Maximum Velocity 1.948E-01

___Scale _ 2.500E+00 (cm.gm.us) CYCLE 1000 T = 9.608E+01

STEEL INTO STEEL PLANAR



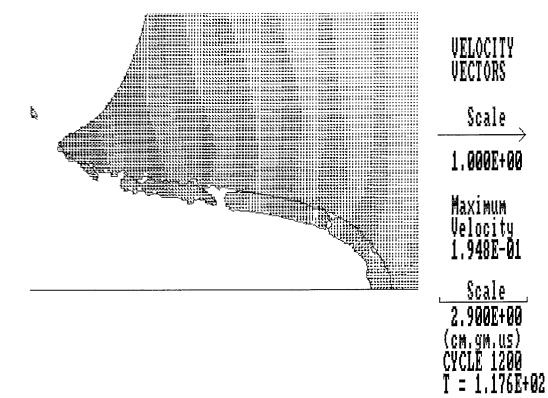
STEEL INTO STEEL PLANAR



HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 1200 T = 1.176E+02

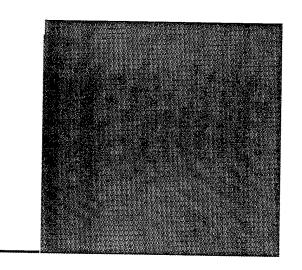
STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

Appendix A6

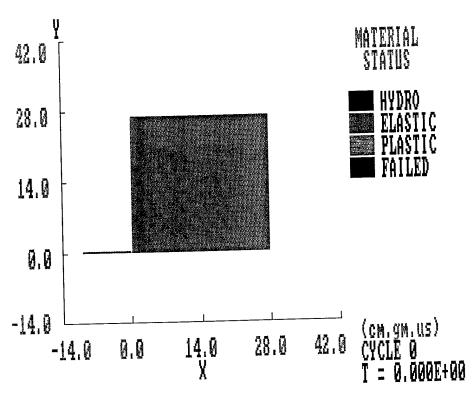
Plots for run No. 6 Steel projectile Planar symmetry 2.5 km/s



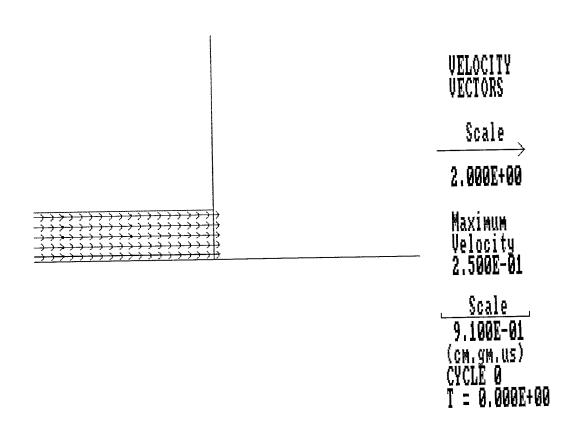


(cm.gm.us) CYCLE 0 T = 0.000E+00

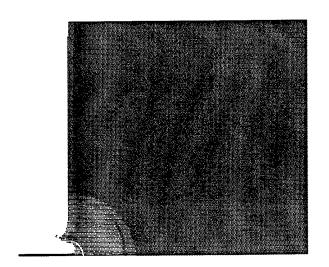
STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR



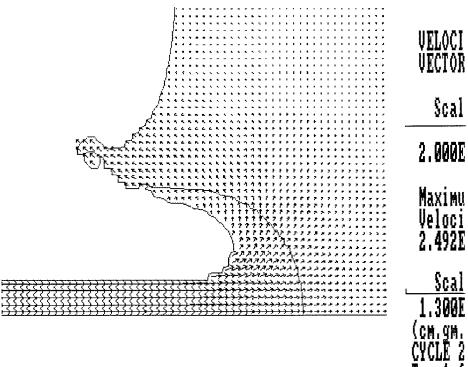
STEEL INTO STEEL PLANAR



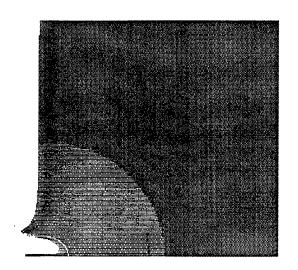
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 200 T = 1.677E+01

STEEL INTO STEEL PLANAR



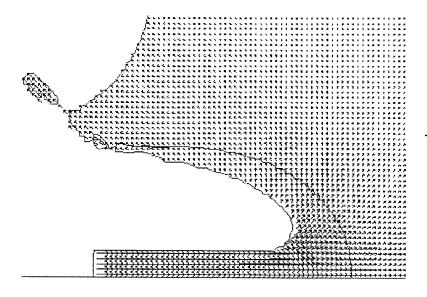
STEEL INTO STEEL PLANAR





(cm.gm.us) CYCLE 400 T = 3.427E+01

STEEL INTO STEEL PLANAR



VELOCITY VECTORS

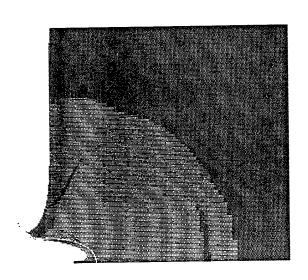
Scale

2.000E+00

Maximum Velocity 2.467E-01

Scale 1.700E+00 (cm.gm.us) CYCLE 400 T = 3.427E+01

STEEL INTO STEEL PLANAR

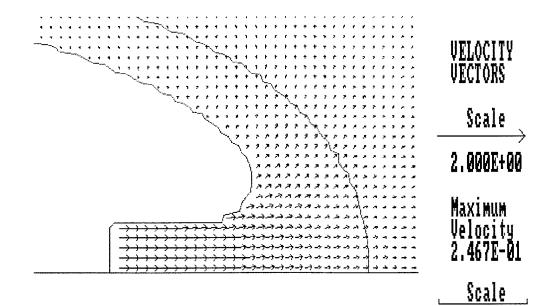


MATERIAL STATUS



(cm.gm.us) CYCLE 600 T = 5.201E+01

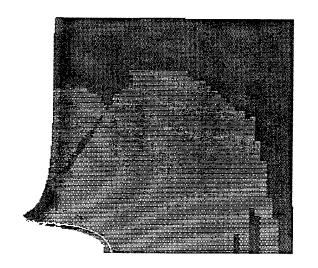
STEEL INTO STEEL PLANAR



9.100E-01

(cm,gm.us) CYCLE 600 T = 5.201E+01

STEEL INTO STEEL PLANAR

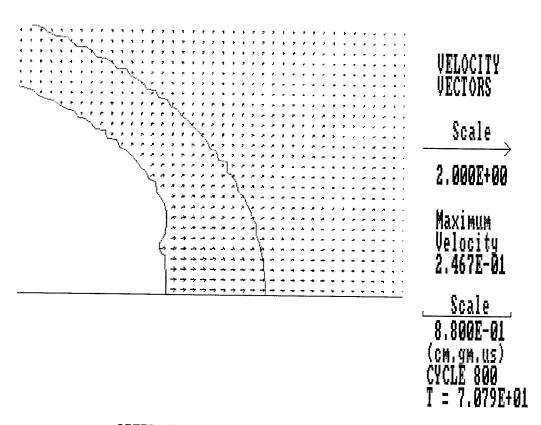


MATERIAL STATUS

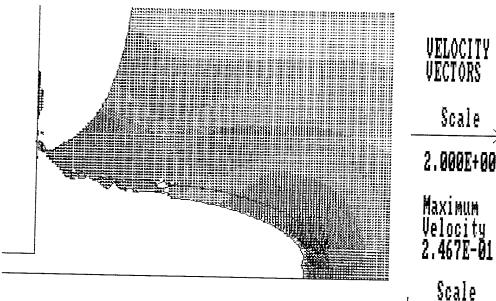
HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 800 T = 7.079E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR



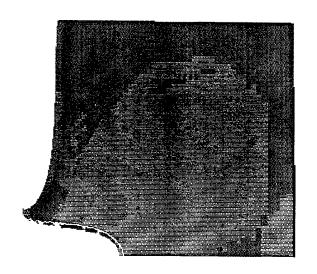
Scale 3.300E+00 (cm.gm.us) CYCLE 800 T = 7.079E+01

VELOCITY VECTORS

Scale

2.000E+00

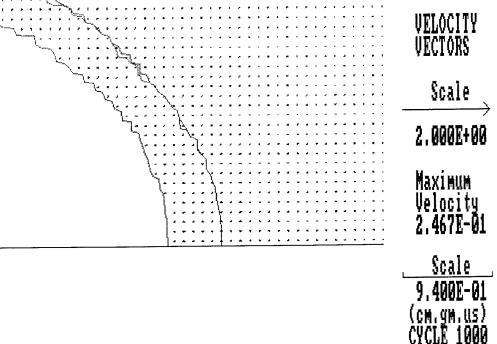
STEEL INTO STEEL PLANAR



HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 1000 T = 9.143E+01

STEEL INTO STEEL PLANAR



STEEL INTO STEEL PLANAR

Appendix A7

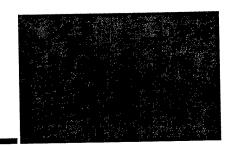
Plots for run No. 7

Tungsten alloy projectile

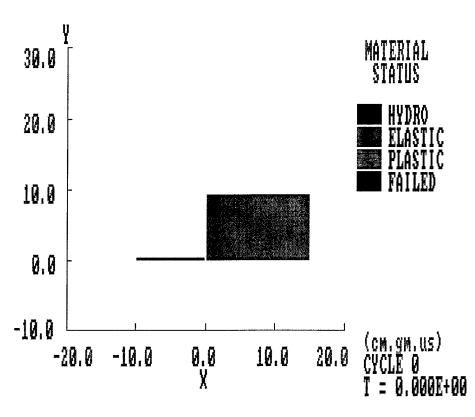
Axial symmetry

1.5 km/s





(cm.gm.us) CYCLE 0 T = 0.000E+00



TUNGSTEN INTO STEEL

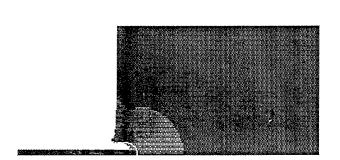
VELOCITY VECTORS

Scale

8.000E-01

Maximum Velocity 1.500E-01

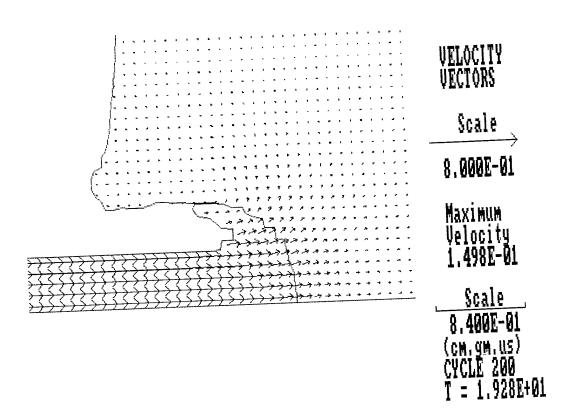
Scale
6.500E-01
(cm.gm.us)
CYCLE 0
T = 0.000E+00



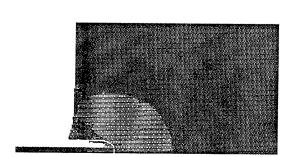
MATERIAL STATUS



(cm.gm.us) CYCLE 200 T = 1.928E+01



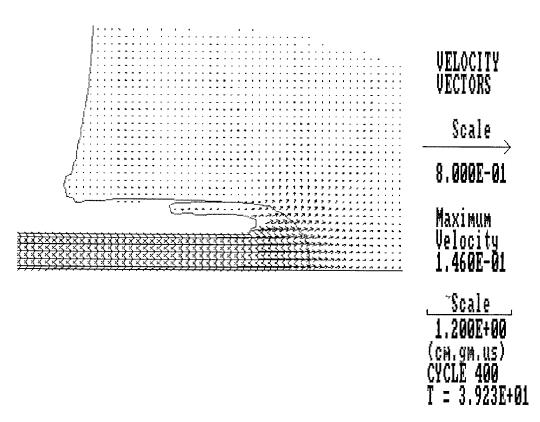
TUNGSTEN INTO STEEL



MATERIAL STATUS



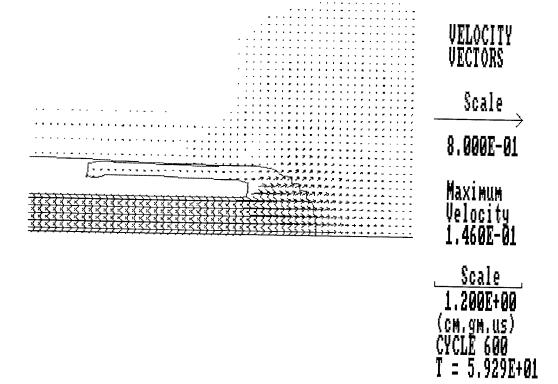
(cm.gm.us) CYCLE 400 T = 3.923E+01



TUNGSTEN INTO STEEL



(cm.gm.us) CYCLE 600 T = 5.929E+01

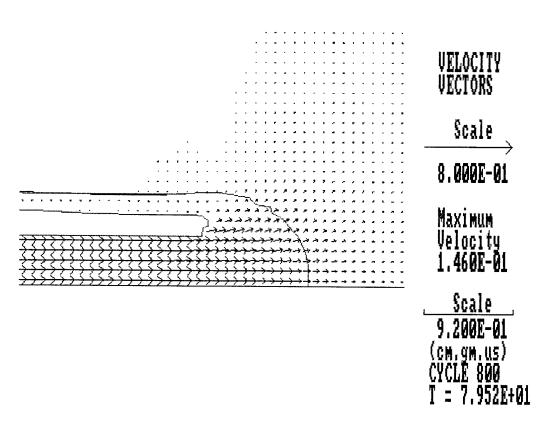


TUNGSTEN INTO STEEL





(cm.gm.us) CYCLE 800 T = 7.952E+01

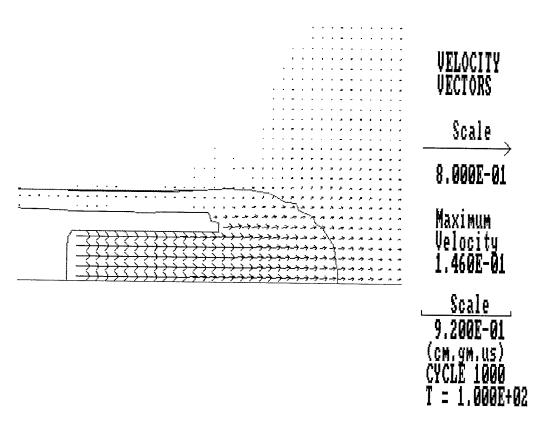


TUNGSTEN INTO STEEL





(cm.gm.us) CYCLE 1000 T = 1.000E+02



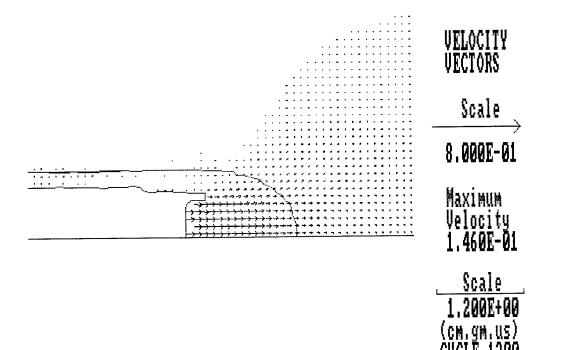
TUNGSTEN INTO STEEL



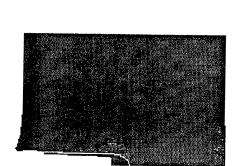




(cm.gm.us) CYCLE 1200 T = 1.214E+02

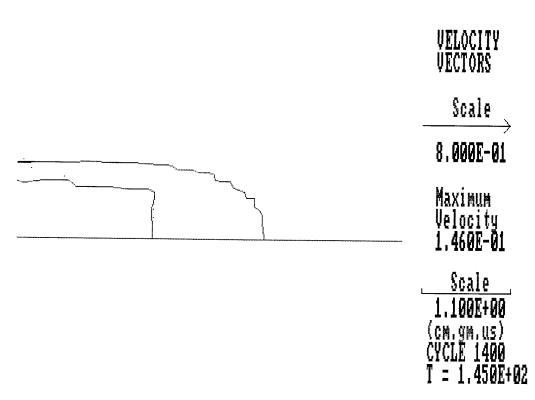


TUNGSTEN INTO STEEL



MATERIAL STATUS HYDRO ELASTIC PLASTIC FAILED

(cm.gm.us) CYCLE 1400 T = 1.450E+02



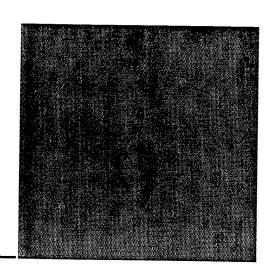
Appendix A8

Plots for run No. 8

Tungsten alloy projectile

Planar symmetry

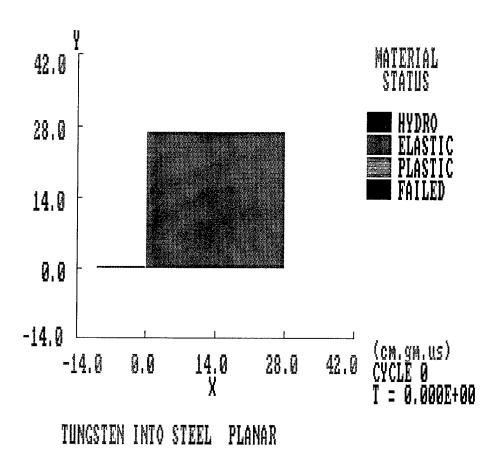
1.5 km/s

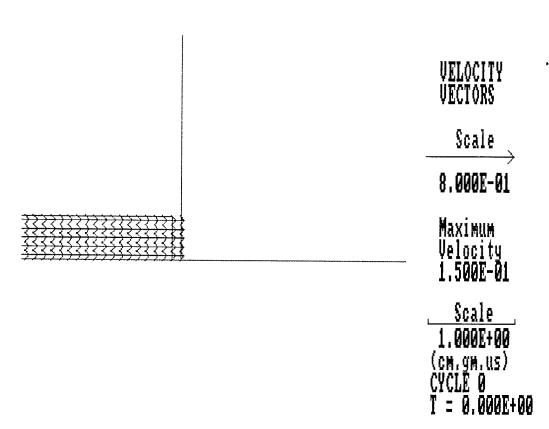




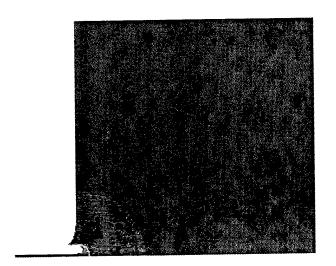
(cm.gm.us) CYCLE 0 T = 0.000E+00

TUNGSTEN INTO STEEL PLANAR





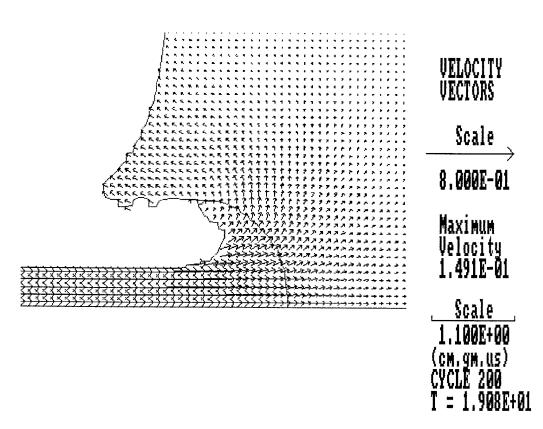
TUNGSTEN INTO STEEL PLANAR



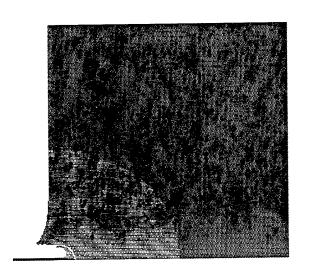


(cm.gm.us) CYCLE 200 T = 1.908E+01

TUNGSTEN INTO STEEL PLANAR



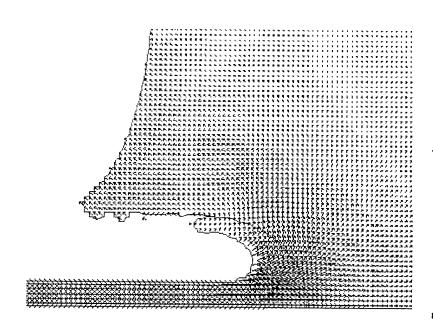
TUNGSTEN INTO STEEL PLANAR





(cm.gm.us) CYCLE 400 T = 3.905E+01

TUNGSTEN INTO STEEL PLANAR



VELOCITY VECTORS

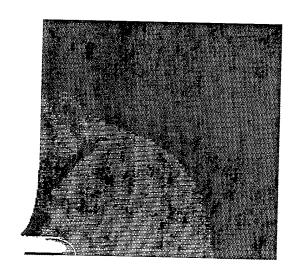
Scale

8.000E-0

Maximum Velocity 1.448E-0

1.800E+0 (cm.gm.us CYCLE 400 T = 3.905

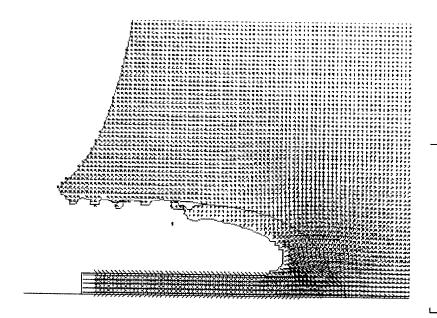
TUNGSTEN INTO STEEL PLANAR





(cm.gm.us) CYCLE 600 T = 5.917E+0

TUNGSTEN INTO STEEL PLANAR



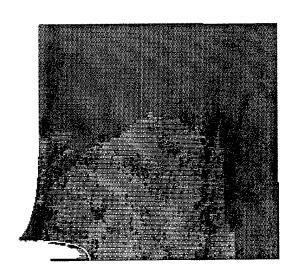
VELOCITY VECTORS

Scale

8.000E-01

Maximum Velocity 1.448E-01

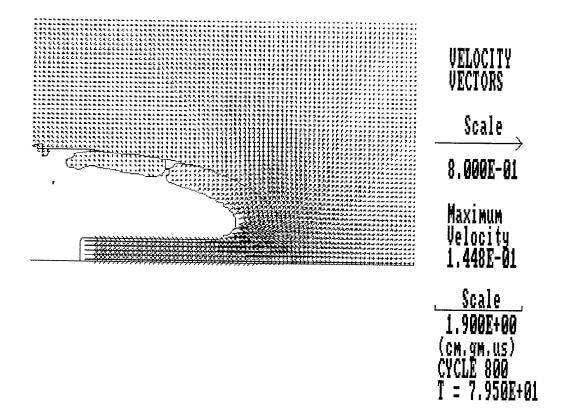
TUNGSTEN INTO STEEL PLANAR





(cm.gm.us) CYCLE 800 T = 7.950E+01

TUNGSTEN INTO STEEL PLANAR



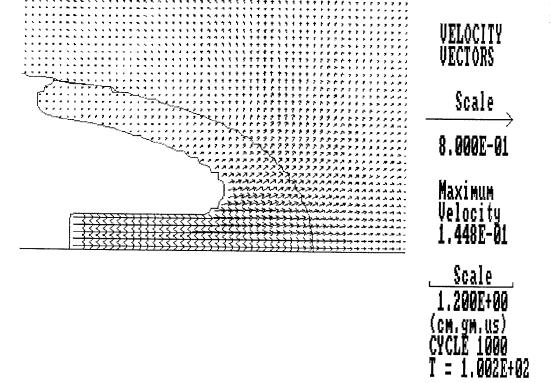
TUNGSTEN INTO STEEL PLANAR





(cm.gm.us) CYCLE 1000 T = 1.002E+02

TUNGSTEN INTO STEEL PLANAR

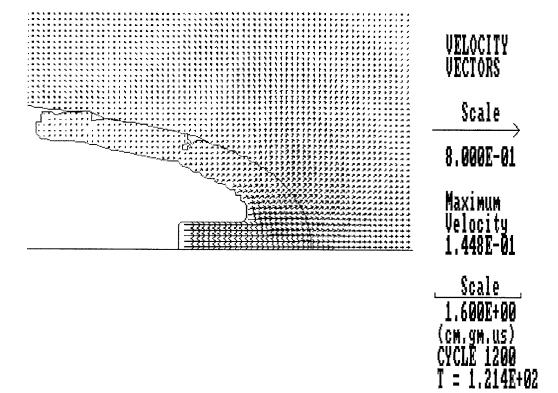


TUNGSTEN INTO STEEL PLANAR

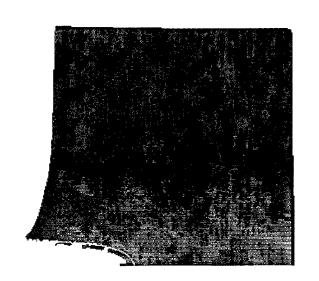


(cm.gm.us CYCLE 120 T = 1.214

TUNGSTEN INTO STEEL PLANAR



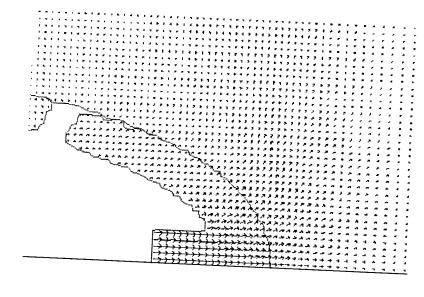
TUNGSTEN INTO STEEL PLANAR



HYDRO
ELASTIC
PLASTIC
FAILED

(cm.gm.us) CYCLE 1400 T = 1.436E+02

TUNGSTEN INTO STEEL PLANAR



VELOCITY VECTORS

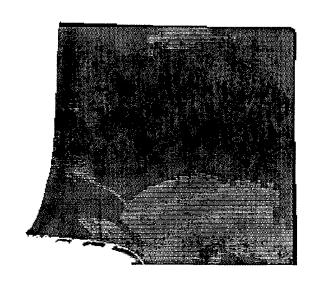
Scale

8.000E-01

Maximum Velocity 1.448E-01

<u>Scale</u> 1.300E+00 (cm.gm.us) CYCLE 1400 T = 1.436E+02

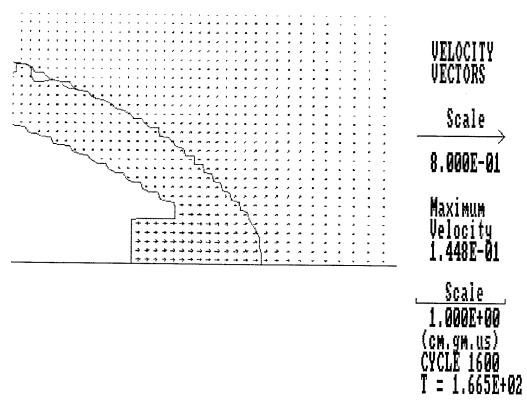
TUNGSTEN INTO STEEL PLANAR





(cm.gm.us) CYCLE 1600 T = 1.665E+02

TUNGSTEN INTO STEEL PLANAR



TUNGSTEN INTO STEEL PLANAR

Appendix B Distribution List

Administrator Defense Technical Information Center Attn: DTIC-DDA 8725 John J. Kingman Road, Ste 0944 Ft. Belvoir, VA 22060-6218

Director US Army Research Lab ATTN: AMSRL OP SD TA 2800 Powder Mill Road Adelphi, MD 20783-1145

Director US Army Research Lab ATTN: AMSRL OP SD TL 2800 Powder Mill Road Adelphi, MD 20783-1145

Director US Army Research Lab ATTN: AMSRL OP SD TP 2800 Powder Mill Road Adelphi, MD 20783-1145

Director Army Research Laboratory AMSRL-CI-LP Technical Library 305 APG, MD 21005-5066